

一类梁的横向振动方程的稳定性分析

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摘 要: 研究了一类梁的横向振动方程的稳定性态, 使用 Galerkin 截断得到仅含时间变量的非线性常微分方程组。利用微分方程稳定性理论, 讨论了系统平衡点的稳定性态。通过对参数的分析, 得到了系统不同类型平衡点的存在条件, 并给出了数值模拟。

关键词: 振动; 稳定性; 平衡点; 极限环

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工程中许多问题都可以归结为梁, 如电线杆、电视发射塔、风力机塔筒等, 但目前对这些结构振动特性的计算都采用有限元方法, 如何快速、准确计算这类结构的振动特性(如固有频率、模态等), 是一个具有工程意义的课题。本文利用数学、力学中的振动分析理论和定性稳定性理论, 对如下一类梁的横向振动方程的稳定性进行了研究:

$$\ddot{w} - \frac{\eta H}{\rho(H+h)(1-v_j^2)} \left(2 \frac{\partial w}{\partial x} \frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial x \partial t} + \left(\frac{\partial w}{\partial x} \right)^2 \frac{\partial^2 w}{\partial x \partial t} \right) + 2V_e \frac{\partial^2 w}{\partial x \partial t} + \frac{\eta H}{12\rho(H+h)(1-V_j^2)} \frac{\partial^5 w}{\partial x^4 \partial t} + \frac{E(h^3 + 3H^2h + 3Hh^2)}{12\rho(H+h)(1-V_e^2)} \frac{\partial^4 w}{\partial x^4} + \frac{E_0H^3}{12\rho(H+h)(1-V_j^2)} \frac{\partial^4 w}{\partial x^4} + V_e^2 \frac{\partial^2 w}{\partial x^2} - \frac{3Eh}{2\rho(H+h)(1-V_e^2)} \left(\frac{\partial w}{\partial x} \right)^2 \frac{\partial^2 w}{\partial x^2} - \frac{3E_0H}{2\rho(H+h)(1-V_j^2)} \left(\frac{\partial w}{\partial x} \right)^2 \frac{\partial^2 w}{\partial x^2} = 0 \quad (1)$$

1 平衡点性态分析

本文只考虑关于 w 的情况, 并令 V_e, V_j 均为 0, 整理得

$$\ddot{w} + 2V_e \frac{\partial^2 w}{\partial x \partial t} + \frac{\eta H}{12\rho(H+h)} \frac{\partial^5 w}{\partial x^4 \partial t} + \left(\frac{E(h^3 + 3H^2h + 3Hh^2)}{12\rho(H+h)} + \frac{E_0H^3}{12\rho(H+h)} \right) \frac{\partial^4 w}{\partial x^4} +$$

$$V_e^2 \frac{\partial^2 w}{\partial x^2} - \frac{3(Eh + E_0H)}{2\rho(H+h)} \left(\frac{\partial w}{\partial x} \right)^2 \frac{\partial^2 w}{\partial x^2} - \frac{\eta H}{\rho(H+h)} \left(2 \frac{\partial w}{\partial x} \frac{\partial^2 w}{\partial x^2} + \left(\frac{\partial w}{\partial x} \right)^2 \right) \frac{\partial^2 w}{\partial x \partial t} = 0 \quad (2)$$

设(2)式有如下级数形式的解

$$w = \sum \varphi_i(x) q_i(t) = \varphi_1(x) q_1(t) + \varphi_2(x) q_2(t) + \dots \quad (3)$$

将(3)式代入(2)式整理得:

$$\sum \varphi_i(x) \dot{q}_i(t) + 2V_e \sum \varphi'_i(x) \dot{q}_i(t) + \frac{\eta H}{12\rho(H+h)} \sum \varphi''_i(x) \dot{q}_i(t) + \left(\frac{E(h^3 + 3H^2h + 3Hh^2)}{12\rho(H+h)} + \frac{E_0H^3}{12\rho(H+h)} \right) \sum \varphi''_i(x) q_i(t) + V_e^2 \sum \varphi'_i(x) q_i(t) - \frac{3(Eh + E_0H)}{2\rho(H+h)} \sum \varphi'_i(x) \varphi'_j(x) \varphi''_k(x) q_i(t) q_j(t) q_k(t) - \frac{\eta H}{\rho(H+h)} \left(2 \sum \varphi'_i(x) \varphi''_j(x) \varphi'_k(x) q_i(t) q_j(t) \dot{q}_k(t) + \sum \varphi'_i(x) \varphi'_j(x) \varphi'_k(x) q_i(t) q_j(t) \dot{q}_k(t) \right) = 0 \quad (4)$$

将(4)式两边同乘 $\varphi_m(x)$, 并在 $[0, a]$ 上对 x 积分, 再令

$$\int_0^a \varphi_i(x) \varphi_m(x) dx = a_{mi}$$

$$\int_0^a \varphi_m(x) \varphi'_i(x) dx = b_{mi}$$

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$$\int_0^a \varphi_m(x) \varphi_i''(x) dx = c_{mi},$$

$$\int_0^a \varphi_m(x) \varphi_i'''(x) dx = d_{mi}$$

$$\int_0^a \varphi_m(x) \varphi_i'(x) \varphi_j(x) \varphi_k''(x) dx = e_{mijk}$$

$$\int_0^a \varphi_i'(x) \varphi_j'(x) \varphi_k'(x) \varphi_m(x) dx = f_{mijk}$$

整理得:

$$\sum a_{mi} \ddot{q}_i(t) + \sum \left[2V_e b_{mi} + \frac{\eta H}{12\rho(H+h)} d_{mi} \right] \dot{q}_i(t) + \sum \left[V_e^2 c_{mi} + \left(\frac{E(h^3 + 3H^2h + 3Hh^2)}{12\rho(H+h)} + \frac{E_0 H^3}{12\rho(H+h)} \right) d_{mi} \right] q_i(t) - \sum \frac{3(Eh + E_0H)}{2\rho(H+h)} e_{mijk} q_i(t) q_j(t) q_k(t) - \sum \left[\frac{\eta H}{\rho(H+h)} (2e_{mijk} + f_{mijk}) \right] q_i(t) q_j(t) \dot{q}_k(t) = 0 \quad (5)$$

根据实际生产的需求,取 $w(x,t) = \sin \frac{\pi}{a} x q_1(t)$,

代入(5)式得

$$\dot{q}_1 + \frac{\eta H \pi^4 q_1}{12\rho(H+h)} - \left[\frac{\pi^2 V_e^2}{a^2} - \frac{\pi^4 (E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3)}{12\rho(H+h)a^4} \right] q_1 + \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} q_1^3 + \frac{\eta H \pi^4}{2\rho(H+h)a^4} q_1^2 \dot{q}_1 = 0 \quad (6)$$

令 $\dot{q}_1 = p_1$, 则(6)式化为如下微分方程组

$$\begin{cases} \dot{q}_1 = -\frac{\eta H \pi^4}{12\rho(H+h)a^4} p_1 + \left[\frac{\pi^2 V_e^2}{a^2} - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^4}{a^4} \right] q_1 \\ - \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} q_1^3 - \frac{\eta H \pi^4}{2\rho(H+h)a^4} p_1^2 q_1 \triangleq P(p_1, q_1) \\ \dot{p}_1 = p_1 \triangleq Q(p_1, q_1) \end{cases} \quad (7)$$

由 $\begin{cases} P(p_1, q_1) = 0 \\ Q(p_1, q_1) = 0 \end{cases}$ 得

$$p_1 = 0, q_1 = 0 \text{ 或}$$

$$q_1 = \pm \sqrt{\frac{8\rho(H+h)a^2 V_e^2 - 2[E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3]}{3(Eh + E_0H)\pi^2}}$$

显然, 当 $V_e^2 > \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$

时, 系统(7)有三个平衡点:

$$O(0,0)$$

$$M_1 \left(0, \sqrt{\frac{8\rho(H+h)a^2 V_e^2 - 2[E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3]}{3(Eh + E_0H)\pi^2}} \right)$$

$$M_2 \left(0, -\sqrt{\frac{8\rho(H+h)a^2 V_e^2 - 2[E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3]}{3(Eh + E_0H)\pi^2}} \right)$$

当 $V_e^2 \leq \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$ 时, 系统(7)有唯一平衡点 $O(0,0)$ 。

定理 1

(1) 当 $V_e^2 > \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$ 时, 平衡点 $O(0,0)$ 为系统(7)的鞍点。

(2) 当 $V_e^2 < \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$ 时,

① 若 $\Psi > 0$, 平衡点 $O(0,0)$ 为系统(7)稳定的结点;

② 若 $\Psi < 0$, 平衡点 $O(0,0)$ 为系统(7)稳定的焦点;

③ 若 $\Psi = 0$, 平衡点 $O(0,0)$ 为系统(7)稳定的退化结点

$$\Psi = \left[\frac{\eta H \pi^4}{12\rho(H+h)a^4} \right]^2 + \frac{4\pi^2 V_e^2}{a^2} - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{3\rho(H+h)} \cdot \frac{\pi^4}{a^4}$$

证明

系统(7)在 $O(0,0)$ 的 Jacobi 矩阵为

$$\begin{pmatrix} -\frac{\eta H \pi^4}{12\rho(H+h)a^4} - \frac{\pi^2 V_e^2}{a^2} - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^4}{a^4} & \\ 1 & 0 \end{pmatrix}$$

$$\begin{cases} p = \frac{\eta H \pi^4}{12\rho(H+h)a^4} > 0, q = -\frac{\pi^2 V_e^2}{a^2} + \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^4}{a^4} \\ p^2 - 4q = \left[\frac{\eta H \pi^4}{12\rho(H+h)a^4} \right]^2 + \frac{\pi^2 V_e^2}{a^2} - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{3\rho(H+h)} \cdot \frac{\pi^4}{a^4} \end{cases}$$

上述矩阵简写为 $\begin{pmatrix} -p & -q \\ 1 & 0 \end{pmatrix}$, 所以,

(1) 当 $V_e^2 > \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$ 时,

$q < 0$, 则平衡点 $O(0,0)$ 为系统(7)的鞍点。

(2) 当 $V_e^2 < \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0 H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$ 时,

$q > 0$ 。

① 若 $\Psi > 0$, 则 $p^2 - 4q > 0, v_1 > 0$ 所以平衡点 $O(0,0)$ 为系统(7)稳定的结点。

② 若 $\Psi < 0$, 则 $p^2 - 4q < 0, \lambda_{1,2} = \frac{-p \pm \sqrt{4q - p^2}i}{2}$ 所以平衡点 $O(0,0)$ 为系统(7)稳定的焦点。

③ 若 $\Psi = 0$, 则 $p^2 - 4q = 0$, $\lambda_{1,2} = \frac{-p}{2} < 0$, $\lambda_{1,2}$

对应的特征向量为 $(-\frac{p}{2} \quad 1)^T$, 所以平衡点 $O(0,0)$ 为系统(7)稳定的退化结点。

定理 2 当 $V_e^2 = \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$

时, 平衡点 $O(0,0)$ 为系统(7)的汇。

证明 当 $V_e^2 = \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$

时, $q = 0$, $\lambda_1 = -p < 0$, $\lambda_2 = 0$, 此时系统(7)变为:

$$\begin{cases} \dot{\bar{q}}_1 = -\frac{\eta H \pi^4}{12\rho(H+h)a^4} p_1 - \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} q_1^3 \\ \quad - \frac{\eta H \pi^4}{2\rho(H+h)a^4} q_1^2 p_1 \\ \bar{q}_1 = p_1 \end{cases} \quad (8)$$

作非退化线性变换

$$\begin{pmatrix} u_1 \\ v_1 \end{pmatrix} = \begin{pmatrix} -1 & -\frac{\eta H \pi^4}{12\rho(H+h)a^4} \\ 1 & 0 \end{pmatrix} \begin{pmatrix} p_1 \\ q_1 \end{pmatrix}$$

即

$$\begin{pmatrix} p_1 \\ q_1 \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\frac{12\rho(H+h)a^4}{\eta H \pi^4} & -\frac{12\rho(H+h)a^4}{\eta H \pi^4} \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \end{pmatrix}$$

系统(8)变为:

$$\begin{cases} \ddot{u}_1 = \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 (u_1 + v_1)^3 + \\ \quad \frac{\eta H \pi^4}{2\rho(H+h)a^4} \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^2 (u_1 + v_1)^2 v_1 \\ \dot{u}_1 = -\frac{\eta H \pi^4}{12\rho(H+h)a^4} v_1 - \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 \\ \quad (u_1 + v_1)^3 - \frac{\eta H \pi^4}{2\rho(H+h)a^4} \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^2 (u_1 + v_1)^2 v_1 \end{cases} \quad (9)$$

中心流形

$$w_{uc}(0,0) = \{(u_1, v_1) \mid v_1 = h(u_1), h(0) = h'(0) = 0\}$$

将 $h(u_1)$ 表示为幂级数

$$h(u_1) = c_2 u_1^2 + c_3 u_1^3 + o(u_1^4) \quad (10)$$

代入

$$h'(u_1) \bar{u}_1 - \bar{v}_1 = 0 \quad (11)$$

得

$$\begin{aligned} & (2c_2 u_1 + 3c_3 u_1 + o(u_1)) \left[\frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \right. \\ & \left. \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 (u_1 + c_2 u_1 + c_3 u_1 + o(u_1))^3 + \right. \\ & \left. \frac{\eta H \pi^4}{2\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^2 \right. \\ & \left. (u_1 + c_2 u_1 + c_3 u_1 + o(u_1))^2 (c_2 u_1 + c_3 u_1 + o(u_1)) \right] + \end{aligned}$$

$$\begin{aligned} & \frac{\eta H \pi^4}{12\rho(H+h)a^4} (c_2 u_1 + c_3 u_1 + o(u_1)) + \\ & \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 \\ & (u_1 + c_2 u_1 + c_3 u_1 + o(u_1))^3 + \\ & \frac{\eta H \pi^4}{2\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^2 \\ & (u_1 + c_2 u_1 + c_3 u_1 + o(u_1))^2 (c_2 u_1 + c_3 u_1 + o(u_1)) = 0 \end{aligned} \quad (12)$$

比较两边的各项系数得

$$c_2 = 0, c_3 = \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^4 > 0$$

故

$$\begin{aligned} h(u_1) &= \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \\ & \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^4 u_1^3 + o(u_1^4) \end{aligned}$$

于是中心流形 $w_{uc}(0,0)$ 上的解满足

$$\dot{u}_1 = \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 u_1^3 + o(u_1^4)$$

在中心流形上的解, 当 $u_1 > 0$ 时, $\dot{u}_1 < 0$, 即当 $t \rightarrow +\infty$ 时, $u_1(t) \rightarrow 0$; 当 $u_1 < 0$ 时, $\dot{u}_1 > 0$, 即当 $t \rightarrow +\infty$ 时, $u_1(t) \rightarrow 0$ 。

求稳定流形

$$w_{sc}(0,0) = \{(u_1, v_1) \mid u_1 = \bar{h}(v_1), \bar{h}(0) = \bar{h}'(0) = 0\}$$

设

$$\bar{h}(v_1) = d_2 v_1 + d_3 v_1 + o(v_1) \quad (13)$$

代入

$$\bar{h}'(v_1) \bar{v}_1 - \bar{u}_1 = 0 \quad (14)$$

得

$$\begin{aligned} & (2d_2 v_1 + 3d_3 v_1 + o(v_1)) \left[-\frac{\eta H \pi^4}{12\rho(H+h)a^4} v_1 - \right. \\ & \left. \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 \right. \\ & \left. (v_1 + d_2 v_1 + d_3 v_1 + o(v_1))^3 - \frac{\eta H \pi^4}{2\rho(H+h)a^4} \cdot \right. \\ & \left. \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^2 (v_1 + d_2 v_1 + d_3 v_1 + o(v_1))^2 v_1 \right] - \\ & \frac{3(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^3 \\ & 3(v_1 + d_2 v_1 + d_3 v_1 + o(v_1))^3 - \frac{\eta H \pi^4}{2\rho(H+h)a^4} \cdot \\ & \left(-\frac{12\rho(H+h)a^4}{\eta H \pi^4}\right)^2 (v_1 + d_2 v_1 + d_3 v_1 + o(v_1))^2 v_1 = 0 \end{aligned} \quad (15)$$

比较两边的各项系数得

$$d_2 = 0$$

$$d_3 = \left[\frac{(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(\frac{12\rho(H+h)a^4}{\eta H\pi^4} \right)^2 - 2 \right] \left(-\frac{12\rho(H+h)a^4}{\eta H\pi^4} \right)^2$$

故

$$\bar{h}(v_1) = \left[\frac{(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(-\frac{12\rho(H+h)a^4}{\eta H\pi^4} \right)^2 - 2 \right] \left(-\frac{12\rho(H+h)a^4}{\eta H\pi^4} \right) v_1 + o(v_1)$$

于是中心流形 $w_{uc}(0,0)$ 上的解满足

$$\bar{v}_1 = -\frac{\eta H\pi^4}{12\rho(H+h)a^4} v_1 + o(v_1)$$

当 $v_1 > 0$ 时, $\bar{v}_1 < 0$, 即当 $t \rightarrow +\infty$ 时, $v_1(t) \rightarrow 0$ 。

当 $v_1 < 0$ 时, $\bar{v}_1 > 0$, 即当 $t \rightarrow +\infty$ 时, $v_1(t) \rightarrow 0$ 。

综上所述: 原点是汇。

定理 3 当 $V_e^2 > \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$

$$\begin{pmatrix} -\frac{\eta H\pi^4}{12\rho(H+h)a^4} v_1 - \frac{\eta H\pi^4}{2\rho(H+h)a^4} \cdot \left(\frac{8\rho(H+h)a^2}{3(Eh + E_0H)\pi^2} \cdot v_e - \frac{2[E(h^3 + 3H^2h + 3Hh^2) + E_0H^3]}{9(Eh + E_0H)} \right) & 1 \\ \frac{\pi^2}{a^2} \cdot v_e - \left(\frac{E(h^3 + 3H^2h + 3Hh^2)}{12\rho(H+h)} + \frac{E_0H^3}{12\rho(H+h)} \right) \frac{\pi^4}{a^4} & \\ -\frac{9(Eh + E_0H)\pi^4}{8\rho(H+h)a^4} \cdot \left(\frac{8\rho(H+h)a^2}{3(Eh + E_0H)\pi^2} \cdot v_e - \frac{2[E(h^3 + 3H^2h + 3Hh^2) + E_0H^3]}{9(Eh + E_0H)} \right) & 0 \end{pmatrix}^T$$

$$\lambda_1 \cdot \lambda_2 = \frac{2\pi^2}{a^2} \cdot v_e - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{6\rho(H+h)}$$

$$\frac{\pi^4}{a^4} = \frac{2\pi^2}{a^2} \left[v_e - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2} \right] > 0$$

$$\lambda_1 + \lambda_2 = -\frac{\eta H\pi^4}{12\rho(H+h)a^4} - \frac{\eta H\pi^4}{2\rho(H+h)a^4} \cdot \frac{8\rho(H+h)a^2}{3(Eh + E_0H)\pi^2}$$

$$\left[v_e - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2} \right] < 0$$

则 $\lambda_1 < 0, \lambda_2 < 0$ 。

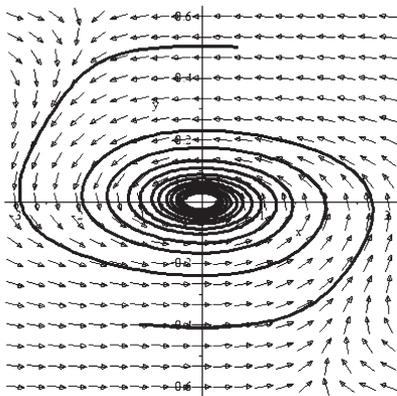


图1 $a_1 = -1, a_2 = -100, a_3 = -50, a_4 = -100$ 系统相图

时,

(1) 若 $\Lambda \geq 0$, 平衡点 M_1, M_2 是系统(7)稳定的结点。

(2) 若 $\Lambda < 0$, 平衡点 M_1, M_2 是系统(7)稳定的焦点。

$$\Lambda = \left(-\frac{\eta H\pi^4}{12\rho(H+h)a^4} - \frac{\eta H\pi^4}{2\rho(H+h)a^4} \cdot \frac{8\rho(H+h)a^2}{3(Eh + E_0H)\pi^2} \left[v_e - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2} \right] \right)^2 - \frac{8\pi^2}{a^2} \left[v_e - \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2} \right]$$

证明 当 $V_e^2 > \frac{E(h^3 + 3H^2h + 3Hh^2) + E_0H^3}{12\rho(H+h)} \cdot \frac{\pi^2}{a^2}$

时, 系统(7)有平衡点 M_1, M_2 , 二者有相同的 Jacobi 矩阵:

所以(1)若 $\Lambda \geq 0$, 平衡点 M_1, M_2 是系统(7)稳定的结点。

(2)若 $\Lambda < 0$, 平衡点 M_1, M_2 是系统(7)稳定的焦点。

2 数值模拟

系统简记为 $\begin{cases} \dot{p}_1 = a_1 p_1 + a_2 q_1 + a_3 q_1^3 + a_4 q_1^5 p_1 \\ \dot{q}_1 = p_1 \end{cases}$, 系统

相图如图1~图4所示。

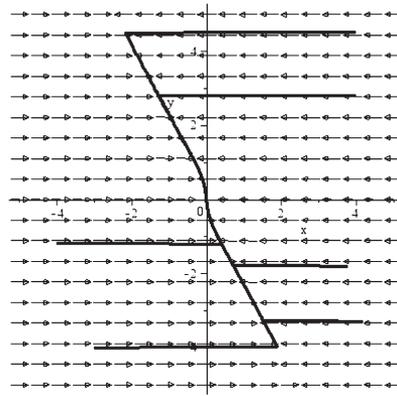
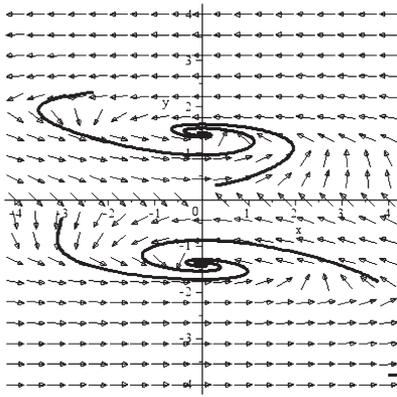
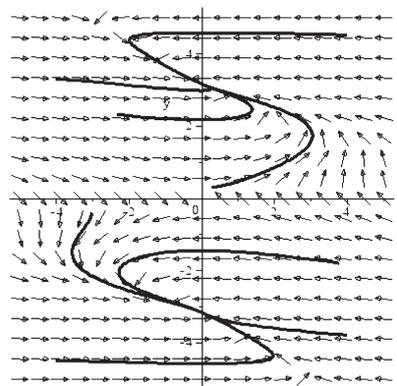


图2 $a_1 = -100, a_2 = -10, a_3 = -50, a_4 = -100$ 系统相图

图 3 $a_1 = -1, a_2 = 10, a_3 = -5, a_4 = -1$ 系统相图图 4 $a_1 = -1, a_2 = 10, a_3 = -1, a_4 = -1$ 系统相图

3 结 论

(1) 使用 Galerkin 截断得到仅含时间变量的非线性

常微分方程组。

(2) 利用微分方程稳定性理论,讨论了系统平衡点的稳定性态,通过对参数的分析,得到了系统不同类型平衡点的存在条件。

(3) 对理论推导进行了数值模拟。

(4) 系统的极限环问题还有待于研究。

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Stability Analysis about the Transverse Vibration Equation of a Beam

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Abstract: The stability condition of the transverse vibration equation about a beam is studied. By using Galerkin truncation, the nonlinear ordinary differential equations only containing the variable time is gotten. We discuss the stability of the system's equilibrium by using of differential equation stability theory. Besides, we can get the existence conditions of different types of the system's equilibrium through the analysis of parameters. The numerical simulation result is also given.

Key words: vibration; stability; equilibrium; limit cycle